

Ta₂O₅–Y₂O₃–ZrO₂ system: Experimental study and preliminary thermodynamic description

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Received 16 June 2010; received in revised form 30 August 2010; accepted 6 September 2010

Available online 16 October 2010

Abstract

Some aspects of stable and equilibrium phases in the Ta₂O₅–Y₂O₃–ZrO₂ system have been studied in this work. Phase stability of Ta_{0.16}Y_{0.16}Zr_{0.68}O₂ and Ta_{0.10}Y_{0.10}Zr_{0.80}O₂ has been studied by X-ray powder diffraction. A secondary phase segregation of YTaO₄ has been observed in both compositions below 1500 °C. However, once treated at 1500 °C, YTaO₄ phase disappears. The preliminary phase diagram of the Ta₂O₅–Y₂O₃–ZrO₂ system at 1200 °C and 1500 °C have been constructed using THERMOCALC package. Thermodynamic description is obtained by critically evaluating experimental data on the binary systems Y₂O₃–Ta₂O₅ and Ta₂O₅–ZrO₂. Binary system data have been combined and parameters for ternary tetragonal and cubic structures have been assessed to construct ternary phase diagram. Calculated isothermal section at 1200 °C is similar to 1500 °C. There is no change in the tetragonal solid solution region observed with temperature, which indicates the same equilibrium phases at 1500 °C and at 1200 °C.

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Keywords: X-ray methods; ZrO₂; Thermal barrier coatings; Phase diagram; Engine component

1. Introduction

New generation of high-efficient gas turbines require new high-temperature stable thermal barrier coating (TBC) materials, which could outperform currently broadly used partially stabilized zirconia (7YSZ, 7–8 wt% Y₂O₃ in ZrO₂). 7YSZ has historically offered the best balance of mechanical and thermal properties needed for gas turbine application. However, 7YSZ formed, for example, under plasma spray conditions consists of predominantly metastable ‘non-transformable’ *t'* phase at room temperature, and undergoes transformation into transformable Y-deficient tetragonal ‘*t*’ and Y-rich cubic ‘*c*’ (fluorite) phases when treated for longer time at and above ~1200 °C: *t'* → *t*+*c*.^{1–3} The transformable *t*-phase of 7YSZ undergoes martensitic transformation to monoclinic phase (*t* → *m*) upon cooling accompanied with detrimental volume

expansion (~4–5%). In the search for new TBC suitable for use above 1200 °C, many researchers have tried further doping the YSZ system, for example, with bigger or smaller cations of rare-earth elements.^{1,3} Ta-doped YSZ, which is stable up to 1500 °C has been reported as one prospective TBC.⁴ The peculiarity of the ZrO₂–YO_{1.5}–TaO_{2.5} system is in strong interaction of Y³⁺ and Ta⁵⁺ cations in tetragonal ZrO₂ matrix, leading to much higher solubility of resulted YTaO₄ species compared to the individual solubility of YO_{1.5} and TaO_{2.5}.^{4–6} The transformability of tetragonal ZrO₂ can be correlated with tetragonality (*c/a* ratio), often used for characterization of YSZ and related systems. This correlation was suggested for classification of oxides into stabilizers (decreasing tetragonality) and destabilizers of *t*-ZrO₂ (increasing tetragonality).⁷

Alloying with Ta₂O₅ decreases stability of both *t*- and *c*-phases in the binary ZrO₂–Y₂O₃ system.^{5,7} This destabilization can be explained by the increase of the lattice distortions due to alloying with Ta₂O₅ (or with other oxides, for example Nb₂O₅ or HfO₂). On the other hand, incorporation of stabilizing oxides such as Y₂O₃ decreases the tetragonal distortion and increases

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the stability of ZrO₂ lattice. Stability of ZrO₂ with Y₂O₃ addition was also related to the formation of oxygen vacancies.⁸

However, doping YTaO₄ into ZrO₂ increases both its tetragonality and stability. Increased stability in this case was explained by defect association of the smaller Ta⁵⁺ and bigger Y³⁺ cations in the ZrO₂ lattice.⁵ It was shown that 20 mol% YTaO₄-stabilized ZrO₂ has a Young's modulus of 150 GPa compared to 200 GPa of 7YSZ. Such a lower modulus and possibility of high coefficient of thermal expansion (CTE) is potential indicator of this system as TBC.

Along with the remarkable phase stability, the YTaO₄-doped ZrO₂ system was also found to be suitable for plasma spraying.⁹ Strong interaction between Y³⁺ and Ta⁵⁺ is beneficial for the TBC applications because it (a) leads to remarkably low thermal conductivity even in absence of oxygen vacancies and (b) could reduce individual activities of cations and hence making Y³⁺ cations less susceptible to reaction with foreign ions such as V⁵⁺. It has been reported that YTaZrO₂ system has higher corrosion resistance against sulfate and vanadate melts as compared to 7YSZ.

It was proposed that 16 mol% YTaO₄ doped ZrO₂ is the best TBC candidate as it has the same stability as 20 mol% YTaO₄ doped zirconia along with sufficiently low thermal conductivity of 2 W/mK and a fracture toughness of 4 MPam^{1/2}, which is twice that of 7YSZ. Besides, 16 mol% YTaO₄ doped ZrO₂ has also shown promise in preliminary burner rig test.⁹

Previous works report the presence of single stable tetragonal solid solution of YTaO₄-ZrO₂ only at and above 1500 °C.⁵ However, presence of YTaO₄ phase below 1500 °C was also reported in some other work.⁴ Interestingly, once a single tetragonal solid solution is formed at 1500 °C, it becomes stable and thereafter YTaO₄ phase separation is not observed even at temperature below 1500 °C.⁴ From these observations it may be concluded that single phase tetragonal TaYSZ achieves stability only at 1500 °C and the equilibrium phases below 1500 °C are still unknown.

In order to investigate the low temperature (1200 °C) equilibrium phases in TaYSZ system, we studied ZrO₂ doped with ~20 mol% YTaO₄ doped ZrO₂ (Y_{0.166}Ta_{0.166}Zr_{0.668}O₂) and ~11 mol% YTaO₄ doped ZrO₂ (Y_{0.1}Ta_{0.1}Zr_{0.8}O₂). Short-time and long-time stability of these systems at 1250 °C have been studied. Previous data about the ZrO₂-Ta₂O₅-Y₂O₃ system and constituent binaries have been reviewed, phases have been modelled by compound energy formalism and a ternary phase diagram has been calculated using Thermo-calc package.^{10,11}

2. Experimental

Starting powders corresponding to Y_{0.166}Ta_{0.166}Zr_{0.668}O₂ and Y_{0.1}Ta_{0.1}Zr_{0.8}O₂ stoichiometries were prepared by reverse co-precipitation technique. Here onward, these two compositions will be named as 20TaYSZ and 11TaYSZ, respectively. ZrOCl₂·8H₂O (99.9%, Alfa-Aesar GmbH, Karlsruhe, Germany), Y(NO₃)₃·6H₂O (99.9%, Alfa-Aesar GmbH, Karlsruhe, Germany) and TaCl₅ (99.99%, Sigma-Aldrich GmbH, Steinheim, Germany) were used as precursors for precipitation of corresponding hydroxides of Zr, Y and Ta, respectively. Precursors

were mixed in ethanol solution and slowly dropped into ammonia solution at pH 10. Precipitates were washed thoroughly, dried overnight and calcined at 1000 °C for 4 h. Calcined powders were annealed at temperatures from 1100 °C to 1500 °C for 4 h. Long-term annealing of the powders was done at 1250 °C for 600 h. For all the heat treatments, heating and cooling rate were maintained at 10 K/min. Phases formed at different temperatures were analysed using X-ray powder diffractometer (Xpert Pro PANalytical, 7600 AA ALMELO, The Netherlands).

3. Thermodynamic assessment of the ZrO₂-Y₂O₃-Ta₂O₅ system

The experimental thermodynamic data and CALPHAD type assessment are not available for ternary ZrO₂-Y₂O₃-Ta₂O₅ system as well as for two constituent binary systems ZrO₂-Ta₂O₅, Y₂O₃-Ta₂O₅ so far. A brief review of all the experimental studies in the binaries and ternaries of this system has been summarised below:

ZrO₂-Ta₂O₅: Only very scarce data are available for phase relations in the ZrO₂-Ta₂O₅ system. Study of Ta₂O₅ rich compositions (5–25 mol% ZrO₂) obtained by solid-state method and heat treated at 1325 and 1410 °C was performed followed by XRD phase identification.¹² At presented schematic diagram, the solubility of ZrO₂ extended up to 10 mol% in the high temperature modification of Ta₂O₅. Several phases with Ta₂O₅/ZrO₂ ratio equal to 6:1, 3:1, 59:6, 27:2, 19:1 and 49:2 were assumed to be stable in the system. A stable orthorhombic phase at Ta₂O₅ concentration of 14.3 mol% was also reported.¹³ Extension of homogeneity range of orthorhombic phase was found to be up to ~33 mol% of Ta₂O₅ in ZrO₂. Later on the stability of orthorhombic phase Ta₂Zr₆O₁₇ with less extensive homogeneity range between 11 and 17 mol% Ta₂O₅ was confirmed as well as maximum solubility of Ta₂O₅ in ZrO₂ at 2 mol%.¹⁴

Y₂O₃-Ta₂O₅: Three stable compounds: Y₃TaO₇ with pyrochlore structure having homogeneity range from 20 to 30 mol% of Ta₂O₅, YTaO₄ with monoclinic to tetragonal transformation at ~1400 °C and YTa₃O₉ with perovskite structure were found as a result of phase equilibria studies in the Y₂O₃-Ta₂O₅ system.¹⁵ All three compounds melt congruently at 2300, 2060 and 1800 °C, respectively. Four eutectic reactions at 2250, 2000, 1700 and 1750 °C were found.¹⁵

Investigation of samples obtained by co-precipitation and heat treated at 1250 and 1590 °C has shown that less than 1 mol% of Y₂O₃ is dissolved in the Ta₂O₅ and up to 5% Ta₂O₅ can be dissolved in the Y₂O₃.¹⁶ Several intermediate compounds were found: YTa₇O₁₉ with tetragonal structure stable up to 1650 °C, YTa₃O₉ with perovskite structure, YTaO₄ with two modifications: monoclinic (low temperature) and tetragonal scheelite type (high temperature) and Y₃TaO₇ with fluorite structure. A new phase, YTa₇O₁₉ was found and crystal structure of Y₃TaO₇ phase as fluorite was determined, which was later confirmed by other investigators.^{15,17,18} Phase relations in the Y₂O₃-Ta₂O₅ system were also studied experimentally by identification of solid-state reaction products with XRD at 1350–1700 °C and liquidus determination by DTA (differential

thermal analysis).^{17,18} Two orthorhombic phases ‘O’ (30 mol% Ta₂O₅) and ‘W2’ (25 mol% Ta₂O₅) were found stable at temperatures up to 1900 and 1600 °C, respectively. The fluorite structure (~20 mol% Ta₂O₅) was found stable at temperature above 1550 °C up to congruent melting (2454 °C). Two eutectic reactions were found: (1) at 2220 °C and 8 mol% of Ta₂O₅ and (2) at 1990 °C and 38 mol% Ta₂O₅. It should be mentioned that temperatures of two eutectic reactions and melting temperature of YTaO₄ are in a good agreement with that reported elsewhere,¹⁵ while the melting temperature of fluorite structure is ~150 K higher than what was reported before (2300 °C).¹⁵ The fluorite and two orthorhombic phases were not distinguished in previous work on Y₂O₃–Ta₂O₅ system¹⁵ and were presented as series of solid solutions with pyrochlore structure. Two Y₂O₃–*x*Ta₂O₅ compounds with *x* = 30 and 21.5 mol% were synthesised by solid-state reaction at 1700 °C, which possess, according to neutron diffraction, orthorhombic and fluorite structures, respectively.¹⁹ Fluorite type phase with 20 mol% of Ta₂O₅ was also obtained earlier.²⁰

ZrO₂–Y₂O₃: One of the authors performed CALPHAD assessment of thermodynamic parameters for the ZrO₂–Y₂O₃ system earlier and presented review of available experimental data (both phase equilibrium data and thermodynamic measurements).^{21–23}

ZrO₂–Y₂O₃–Ta₂O₅: Phases in the ZrO₂–Ta₂O₅–Y₂O₃, obtained by co-precipitation and heat treated at 1500 °C,⁵ were identified by XRD. It was shown that tetragonal ZrO₂ based solid solution was single phase up to 22 mol% of YTaO₄ in the join ZrO₂–YTaO₄. Two phase field of tetragonal ZrO₂ based solid solution and scheelite was stable up to 80 mol% of YTaO₄. Based on experimental studies the isothermal section was constructed up to 50 mol% of Ta₂O₅. The tetragonal TaYSZ phase containing 20 mol% of YTaO₄ (equal fractions of YO_{1.5} and TaO_{2.5} of 16.6 mol%) was found to be non-transformable.⁴ When the TaO_{2.5} addition to 7YSZ exceeds 4 mol%, single tetragonal phase is stable but transformable to monoclinic on cooling. At higher TaO_{2.5} content of 16–22 mol%, tetragonal phase becomes non-transformable.

Thermodynamic modelling: The solid solution phases (fluorite, tetragonal, cubic Y₂O₃) are described by the compound energy formalism.²⁴ The liquid phase is described by the two-sublattice ionic liquid model,²⁴ with the first sublattice filled by cations and the second one filled by anions, vacancies and neutral species. This study does not consider the metal-rich part of the system and vacancies are not included in the liquid description. The liquid is thus described by the formula (Ta⁴⁺, Y⁵⁺, Zr⁴⁺)_P(O²⁻)_Q, where *P* and *Q* are the number of sites on the cation and anion sublattices, respectively. The stoichiometric factors *P* and *Q* are varied with the composition in order to maintain electroneutrality. The remaining phases (YTaO₄ and δ-Zr₃Y₄O₁₂) are treated as stoichiometric compounds. The Gibbs energy of a solution phase with mixing in two sublattices (i.e. F, T, M, C, H) is expressed as

$$G = \sum_i \sum_j Y_i^s Y_j^t G_{i,j} + RT \sum_s \alpha_s \sum_i Y_i^s \ln Y_i^s + \Delta G^{\text{ex}} \quad (1)$$

where Y_i^s is the mole fraction of a constituent *i* in sublattice *s*, $G_{i,j}$ is Gibbs energy of a compound formed from species *i* and *j*, α_s is the number of sites on the sublattice *s* per mole of formula units of phase and ΔG^{ex} is the excess Gibbs energy of mixing expressed as

$$\Delta G^{\text{ex}} = \sum_s Y_i^s Y_j^s L_{i,j}^s + \Delta G^{\text{tern}} \quad (2)$$

where,

$$L_{i,j}^s = \sum_n (Y_i^s - Y_j^s)^n L_{i,j}^n \quad (3)$$

are the binary interaction parameters in the sublattice *s* and ΔG^{tern} is the contribution of high-order interactions. As a first approximation, the ternary and quaternary interaction parameters for the solid phases are neglected.

Thermodynamic description of the ZrO₂–Y₂O₃ system is accepted from previous work of one of the authors.²³ The thermodynamic data for the Ta₂O₅ are accepted from SGTE substance database [www.sgte.org]. Only one modification of YTaO₄ phase is considered in present work, because of lack of data. Heat capacity (*C_p*) of YTaO₄ phase is described as sum of *C_p* for oxides. Orthorhombic ZrO₂–14.3 mol.% Ta₂O₅ phase is not modelled because its stability limits are not known. Two orthorhombic phases found in the Y₂O₃–Ta₂O₅ system¹⁷ are also not considered because of a lack of data. The fluorite and tetragonal solid solutions are presented by different formulae in the ZrO₂–Y₂O₃ and ZrO₂–Ta₂O₅ systems to keep electroneutrality. The formulae are following: (Zr⁴⁺, Y³⁺)(O²⁻, Va)₂ and (Zr⁴⁺, Ta⁵⁺, Va)(O²⁻)₂, respectively. Therefore, in ternary system, the formula for fluorite and tetragonal solid solutions should be presented as (Zr⁴⁺, Ta⁵⁺, Y³⁺, Va)(O²⁻, Va)₂, to be consistent with binary systems. The models and list of parameters used to describe phases in the ZrO₂–Ta₂O₅–Y₂O₃ system are presented in Table 1.

4. Results and discussion

4.1. Experimental results

X-ray diffraction patterns of 20TaYSZ annealed at different temperatures are shown in Fig. 1. Broad diffraction peaks indicate nanocrystalline nature of the 20TaYSZ powder annealed at 1100 °C. Nanocrystallinity is well known property of oxide powders obtained using solution chemistry routes. Diffraction peaks become sharper after treatment at 1200 °C, indicating crystallite growth with temperature. A secondary phase of m-YTaO₄ is clearly visible in all samples treated at temperatures below 1500 °C. YTaO₄ phase disappears at 1500 °C. This observation has been previously reported⁴ and is also consistent with the phase diagram proposed by Kim and Tien.⁵ It seems that single stable tetragonal phase forms only at 1500 °C. It is possible to see, that tetragonality of the 20TaYSZ increases with temperature (Table 2) and at 1500 °C reaches a value, which is much higher than the maximum value of 1.0203 acceptable or possible for room temperature stable phase of t-ZrO₂.⁵ This means that solubility of YTaO₄ into ZrO₂ lattice increases with temperature

Table 1
Thermodynamic parameters for phases in the ZrO_2 – Ta_2O_5 – Y_2O_3 system.

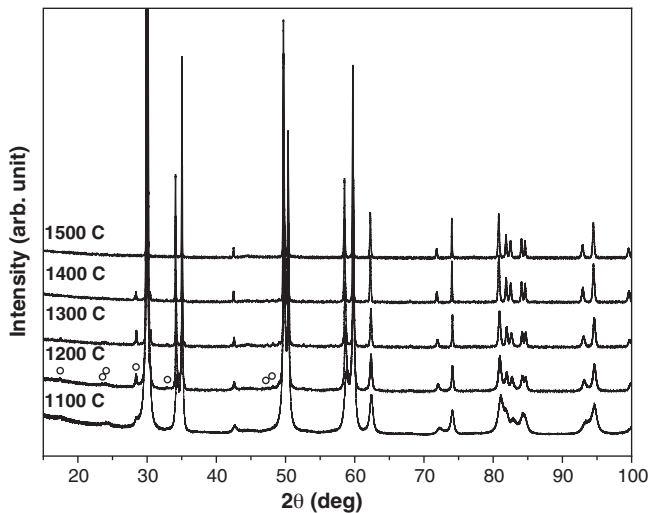
Phase/temperature range	Model/parameter
IONIC_LIQUID 298.15–4000	$(Ti^{5+}, Y^{3+}, Zr^{4+})(O^{2-})_2$ $G(IONIC_LIQUID, Ta^{5+}:O^{2-}) = GTA2O5 + 122000 - 57.0386932 \cdot T$ $G(IONIC_LIQUID, Zr^{4+}:O^{2-}) = 2 \cdot GZRO2L$ $G(IONIC_LIQUID, Y^{3+}:O^{2-}) = GY2O3R + 108779 - 40.509 \cdot T$ ${}^0L(IONIC_LIQUID, Y^{3+}, Zr^{4+}:O^{2-}) = 11488.4008$ ${}^1L(IONIC_LIQUID, Y^{3+}, Zr^{4+}:O^{2-}) = 1608.38521$
Y2O3_CUB 298.15–6000	$(Y^{3+}, Zr^{4+}, Ta^{5+}, Va)(O^{2-})_3 (O^{2-}, Va)$ $G(Y2O3_CUB, Zr^{4+}:O^{2-}:O^{2-}) = 2 \cdot GZRO2C;$ $G(Y2O3_CUB, Zr^{4+}:O^{2-}:Va) = 2 \cdot GZRO2C - GHSEROO$ $G(Y2O3_CUB, Y^{3+}:O^{2-}:O^{2-}) = GY2O3R + GHSEROO$ $G(Y2O3_CUB, Y^{3+}:O^{2-}:Va) = +GY2O3R$ $G(Y2O3_CUB, Ta^{5+}:O^{2-}:O^{2-}) = GTA2O5 - GHSEROO + 10.401375 \cdot T - 10000$ $G(Y2O3_CUB, Ta^{5+}:O^{2-}:Va) = GTA2O5 - 2 \cdot GHSEROO - 20000 + 10.40135 \cdot T$ $G(Y2O3_CUB, Va:O^{2-}:Va) = 3 \cdot GHSEROO + 30000$ $G(Y2O3_CUB, Va:O^{2-}:O^{2-}) = 4 \cdot GHSEROO + 40000$ ${}^0L(Y2O3_CUB, Y^{3+}, Zr^{4+}:O^{2-}:O^{2-}) = -34451.2175 + 39.5035342 \cdot T$ ${}^0L(Y2O3_CUB, Y^{3+}, Zr^{4+}:O^{2-}:Va) = -34451.2175 + 39.5035342 \cdot T$ ${}^0L(Y2O3_CUB, Zr^{4+}, Ta^{5+}:O^{2-}:O^{2-}) = 120000$ ${}^0L(Y2O3_CUB, Zr^{4+}, Ta^{5+}:O^{2-}:Va) = 120000$ ${}^0L(Y2O3_CUB, Va, Zr^{4+}:O^{2-}:O^{2-}) = 120000$ ${}^0L(Y2O3_CUB, Va, Zr^{4+}:O^{2-}:Va) = 120000$ ${}^0L(Y2O3_CUB, Va, Ta^{5+}:O^{2-}:O^{2-}) = 120000$ ${}^0L(Y2O3_CUB, Va, Ta^{5+}:O^{2-}:Va) = 120000$ ${}^0L(Y2O3_CUB, Va, Y^{3+}:O^{2-}:O^{2-}) = 120000$ ${}^0L(Y2O3_CUB, Va, Y^{3+}:O^{2-}:Va) = 120000$ ${}^0L(Y2O3_CUB, Ta^{5+}, Y^{3+}:O^{2-}:O^{2-}) = 120000$ ${}^0L(Y2O3_CUB, Ta^{5+}, Y^{3+}:O^{2-}:Va) = 120000$ ${}^0L(Y2O3_CUB, Y^{3+}, Zr^{4+}, Ta^{5+}:O^{2-}:O^{2-}) = 200000$ ${}^0L(Y2O3_CUB, Y^{3+}, Zr^{4+}, Ta^{5+}:O^{2-}:Va) = 200000$
Y2O3_HEX 298.15–6000	$(Y^{3+}, Zr^{4+})_2 (O^{2-})_3 (O^{2-}, Va)$ $G(Y2O3_HEX, Zr^{4+}:O^{2-}:O^{2-}) = 2 \cdot GZRO2C + 50000$ $G(Y2O3_HEX, Zr^{4+}:O^{2-}:Va) = 2 \cdot GZRO2C - GHSEROO + 50000$ $G(Y2O3_HEX, Y^{3+}:O^{2-}:O^{2-}) = GY2O3H + GHSEROO$ $G(Y2O3_HEX, Y^{3+}:O^{2-}:Va) = GY2O3H$ ${}^0L(Y2O3_HEX, Y^{3+}, Zr^{4+}:O^{2-}:O^{2-}) = 180000$ ${}^0L(Y2O3_HEX, Y^{3+}, Zr^{4+}:O^{2-}:Va) = 180000$
TA2O5_S 298.15–6000	$(Ta^{5+})_2 (O^{2-})_5$ $G(TA2O5_S, Ta^{5+}:O^{2-}) = GTA2O5$
TA2O5_S2 298.15–6000	$(Ta^{5+})_2 (O^{2-})_5$ $G(TA2O5_S2, Ta^{5+}:O^{2-}) = GTA2O5 + 2000 - 1.22473974 \cdot T$
ZRO2_FLU 298.15–6000	$(Ti^{4+}, Y^{3+}, Zr^{4+}, Va)(O^{2-}, Va)_2$ $G(ZRO2_FLU, Zr^{4+}:O^{2-}) = GZRO2C$ $G(ZRO2_FLU, Zr^{4+}:Va) = GZRO2C - 2 \cdot GHSEROO$ $G(ZRO2_FLU, Va:Va) = 0$ $G(ZRO2_FLU, Va:O^{2-}) = 2 \cdot GHSEROO + 600000$ $G(ZRO2_FLU, Ta^{5+}:O^{2-}) = 0.5 \cdot GTA2O5 - 0.5 \cdot GHSEROO + 5.20069 \cdot T - 1.5E5 + 2.2E5$ $G(ZRO2_FLU, Ta^{5+}:Va) = 0.5 \cdot GTA2O5 - 2.5 \cdot GHSEROO + 5.20069 \cdot T - 7.5E5 + 2.2E5$ $G(ZRO2_FLU, Y^{3+}:O^{2-}) = 0.5 \cdot GY2O3R + 2000 + 0.5 \cdot GHSEROO + 9.3511 \cdot T$ $G(ZRO2_FLU, Y^{3+}:Va) = 0.5 \cdot GY2O3R + 2000 - 1.5 \cdot GHSEROO + 9.3511 \cdot T$ ${}^0L(ZRO2_FLU, Y^{3+}, Zr^{4+}:O^{2-}) = -65401.3858 + 25.099522 \cdot T$ ${}^0L(ZRO2_FLU, Y^{3+}, Zr^{4+}:Va) = -65401.3858 + 25.099522 \cdot T$ ${}^1L(ZRO2_FLU, Y^{3+}, Zr^{4+}:O^{2-}) = 67041.1965 - 21.0271896 \cdot T$ ${}^1L(ZRO2_FLU, Y^{3+}, Zr^{4+}:Va) = 67041.1965 - 21.0271896 \cdot T$ ${}^0L(ZRO2_FLU, Ta^{5+}, Y^{3+}:O^{2-}) = 138650 - 50T$ ${}^0L(ZRO2_FLU, Ta^{5+}, Y^{3+}:Va) = 138650 - 50T$ ${}^0L(ZRO2_FLU, Ta^{5+}, Zr^{4+}:O^{2-}) = -140000$ ${}^0L(ZRO2_FLU, Ta^{5+}, Zr^{4+}:Va) = -140000$ ${}^0L(ZRO2_FLU, Ta^{5+}, Va:O^{2-}) = 50000$

Table 1 (Continued)

Phase/temperature range	Model/parameter
ZRO2_TETR 298.15–6000	${}^0L(\text{ZRO2_FLU}, \text{Ta}^{5+}, \text{Va}: \text{Va}) = 50000$ ${}^0L(\text{ZRO2_FLU}, \text{Va}, \text{Zr}^{4+}: \text{O}^{2-}) = -100000$ ${}^0L(\text{ZRO2_FLU}, \text{Va}, \text{Zr}^{4+}: \text{Va}) = -100000$ ${}^0L(\text{ZRO2_FLU}, \text{Va}, \text{Y}^{3+}: \text{O}^{2-}) = 50000$ ${}^0L(\text{ZRO2_FLU}, \text{Va}, \text{Y}^{3+}: \text{Va}) = 50000$ ${}^0L(\text{ZRO2_FLU}, \text{Ta}^{5+}, \text{Y}^{3+}, \text{Zr}^{4+}: \text{O}^{2-}) = 60000$ ${}^0L(\text{ZRO2_FLU}, \text{Ta}^{5+}, \text{Y}^{3+}, \text{Zr}^{4+}: \text{Va}) = 60000$ $(\text{Ta}^{5+}, \text{Y}^{3+}, \text{Zr}^{4+}, \text{Va}) (\text{O}^{2-}, \text{Va})_2$ $G(\text{ZRO2_TETR}, \text{Zr}^{4+}: \text{O}^{2-}) = \text{GZRO2T}$ $G(\text{ZRO2_TETR}, \text{Zr}^{4+}: \text{Va}) = \text{GZRO2T} - 2 \cdot \text{GHSEROO}$ $G(\text{ZRO2_TETR}, \text{Ta}^{5+}: \text{O}^{2-}) = 0.5 \cdot \text{GTa2O5} - 0.5 \cdot \text{GHSEROO}$ $+ 5.20069 \cdot T - 150000 - 220000$ $G(\text{ZRO2_TETR}, \text{Ta}^{5+}: \text{Va}) = 0.5 \cdot \text{GTa2O5} - 2.5 \cdot \text{GHSEROO}$ $+ 5.20069 \cdot T - 750000 - 220000$ $G(\text{ZRO2_TETR}, \text{Y}^{3+}: \text{O}^{2-}) = 0.5 \cdot \text{GY2O3R} + 10000 + 0.5 \cdot \text{GHSEROO}$ $+ 9.3511 \cdot T$ $G(\text{ZRO2_TETR}, \text{Y}^{3+}: \text{Va}) = 0.5 \cdot \text{GY2O3R} + 10000 - 1.5 \cdot \text{GHSEROO}$ $+ 9.3511 \cdot T$ $G(\text{ZRO2_TETR}, \text{Va}: \text{Va}) = 0$ $G(\text{ZRO2_TETR}, \text{Va}: \text{O}^{2-}) = 2 \cdot \text{GHSEROO} + 600000$ $L(\text{ZRO2_TETR}, \text{Y}^{3+}, \text{Zr}^{4+}: \text{O}^{2-}) = -63233.7083 + 30 \cdot T$ $L(\text{ZRO2_TETR}, \text{Y}^{3+}, \text{Zr}^{4+}: \text{Va}) = -63233.7083 + 30 \cdot T$ $L(\text{ZRO2_TETR}, \text{Ta}^{5+}, \text{Zr}^{4+}: \text{O}^{2-}) = -160000$ $L(\text{ZRO2_TETR}, \text{Ta}^{5+}, \text{Zr}^{4+}: \text{Va}) = -160000$ $L(\text{ZRO2_TETR}, \text{Ta}^{5+}, \text{Va}: \text{O}^{2-}) = 40000$ $L(\text{ZRO2_TETR}, \text{Ta}^{5+}, \text{Va}: \text{Va}) = 40000$ $L(\text{ZRO2_TETR}, \text{Va}, \text{Zr}^{4+}: \text{O}^{2-}) = -100000$ $L(\text{ZRO2_TETR}, \text{Va}, \text{Zr}^{4+}: \text{Va}) = -100000$ $L(\text{ZRO2_TETR}, \text{Va}, \text{Y}^{3+}: \text{O}^{2-}) = 50000$ $L(\text{ZRO2_TETR}, \text{Va}, \text{Y}^{3+}: \text{Va}) = 50000$ $L(\text{ZRO2_TETR}, \text{Ta}^{5+}, \text{Y}^{3+}: \text{O}^{2-}) = 50000$ $L(\text{ZRO2_TETR}, \text{Ta}^{5+}, \text{Y}^{3+}: \text{Va}) = 50000$ $L(\text{ZRO2_TETR}, \text{Ta}^{5+}, \text{Y}^{3+}, \text{Zr}^{4+}: \text{O}^{2-}) = -100000$ $L(\text{ZRO2_TETR}, \text{Ta}^{5+}, \text{Y}^{3+}, \text{Zr}^{4+}: \text{Va}) = -100000$
ZRO2_MONO 298.15–6000	$(\text{Y}^{3+}, \text{Zr}^{4+}) (\text{O}^{2-}, \text{Va})_2$ $G(\text{ZRO2_MONO}, \text{Zr}^{4+}: \text{O}^{2-}) = \text{GZRO2M}$ $G(\text{ZRO2_MONO}, \text{Zr}^{4+}: \text{Va}) = \text{GZRO2M} - 2 \cdot \text{GHSEROO}$ $G(\text{ZRO2_MONO}, \text{Y}^{3+}: \text{O}^{2-}) = 0.5 \cdot \text{GY2O3R} + 26900 + 0.5 \cdot \text{GHSEROO}$ $+ 25.4 \cdot T + 9.3511 \cdot T$ $G(\text{ZRO2_MONO}, \text{Y}^{3+}: \text{Va}) = 0.5 \cdot \text{GY2O3R} + 26900 - 1.5 \cdot \text{GHSEROO}$ $+ 25.4 \cdot T + 9.3511 \cdot T$
ZR3Y4O12(δ) 298.15–6000 YTaO4	$(\text{Zr}^{4+})_3(\text{Y}^{3+})_4(\text{O}^{2-})_{12}$ $G(\text{ZR3Y4O12}, \text{Zr}^{4+}: \text{Y}^{3+}: \text{O}^{2-}) = 7 \cdot \text{GZYO}$ $(\text{Y}^{3+})_1(\text{Ta}^{5+})(\text{O}^{2-})_4$ $G(\text{YTaO4}) = 0.5 \cdot \text{GY2O3R} + 0.5 \cdot \text{GTa2O5} - 38000 + 2.5 \cdot T$
Functions 298.15–1300	$\text{GHSEROO} = -7285.88839 + 119.139649 \cdot T - 23.75926 \cdot T \cdot \ln(T)$ $- 0.0026230335 \cdot T^2 + 1.70108833 \cdot 10^{-7} \cdot T^3 - 3292.808/T$
1300–2500	$- 22389.9623 + 243.886592 \cdot T - 41.13709 \cdot T \cdot \ln(T) + 0.00616757 \cdot T^2$ $- 6.55135667 \times 10^{-7} \cdot T^3 + 2429586/T$
2500–3290	$+ 229382.916 - 722.597463 \cdot T + 78.52448 \cdot T \cdot \ln(T) - 0.017983375 \cdot T^2$ $+ 1.95033 \cdot 10^{-7} \cdot T^3 - 93813650/T$
3290–6000	$- 42882.7013 + 269.225623 \cdot T - 41.84 \cdot T \cdot \ln(T)$
298.15–1000	$\text{GHSEROO} = -3480.87 - 25.503038 \cdot T - 11.1355 \cdot T \cdot \ln(T)$ $- 0.005098875 \cdot T^2 + 6.61845833 \cdot 10^{-7} \cdot T^3 - 38365/T$
1000–3300	$- 6568.763 + 12.659879 \cdot T - 16.8138 \cdot T \cdot \ln(T) - 5.957975 \times 10^{-4} \cdot T^2$ $+ 6.781E - 09 \cdot T^3 + 262905/T$
3300–6000	$- 13986.728 + 31.259624 \cdot T - 18.9536 \cdot T \cdot \ln(T) - 4.25243 \times 10^{-4} \cdot T^2$ $+ 1.0721 \times 10^{-8} \cdot T^3 + 4383200/T$
298.15–1000	$\text{GHSERYO} = -8011.09379 + 128.572856 \cdot T - 25.6656992 \cdot T \cdot \ln(T)$ $- 0.00175716414 \cdot T^2 - 4.17561786 \cdot 10^{-7} \cdot T^3 + 26911.509/T$

Table 1 (Continued)

Phase/temperature range	Model/parameter
1000–1795.15	$-7179.74574 + 114.497104 \cdot T - 23.4941827 \cdot T \cdot \ln(T) - 0.0038211802 \cdot T^2 - 8.2534534 \times 10^{-8} \cdot T^3$
1795.15–3700	$-67480.7761 + 382.124727 \cdot T - 56.9527111 \cdot T \cdot \ln(T) + 0.00231774379 \cdot T^2 - 7.22513088 \cdot 10^{-8} \cdot T^3 + 18077162.6/T$
298.15–2128	$\text{GHSEZR} = -7827.595 - 125.64905 \cdot T - 24.1618 \cdot T \cdot \ln(T) - 0.00437791 \cdot T^2 + 34971/T$
2128–6000	$-26085.921 + 2622.724183 \cdot T - 42.144 \cdot T \cdot \ln(T) - 1.342895 \cdot 10^{-31} \cdot T^{-9}$
298.15–1633	$\text{GTa}_2\text{O}_5 = -2103104.07 + 893.195926 \cdot T - 151.255 \cdot T \cdot \ln(T) - 0.015530075 \cdot T^2 - 1.40927433 \times 10^{-10} \cdot T^3 + 1136975/T$
1633–2150	$-2156227.05 + 1335.39795 \cdot T - 210 \cdot T \cdot \ln(T) + 1.6681945 \times 10^{-14} \cdot T^2 - 1.104863 \times 10^{-18} \cdot T^3 + 1.3622705 \times 10^{-5}/T$
2150–6000	$-2177727.05 + 1422.13018 \cdot T - 220 \cdot T \cdot \ln(T) + 1.7185345 \times 10^{-16} \cdot T^2 - 5.45587 \times 10^{-21} \cdot T^3 + 4.627957 \times 10^{-7}/T$
298.15–6000	$\text{GZRO}_2\text{M} = -1126163.54 + 424.890806 \cdot T - 69.3875137 \cdot T \cdot \ln(T) - 0.00375880141 \cdot T^2 + 683000/T$
298.15–6000	$\text{GZRO}_2\text{T} = \text{GZRO}_2\text{M} + 5468 - 4.0 \cdot T$
298.15–6000	$\text{GZRO}_2\text{C} = \text{GZRO}_2 + 10336 - 4.0 \cdot T$
298.15–6000	$\text{GZRO}_2\text{L} = \text{GZRO}_2 + 87027 - 29.17432 \cdot T$
298.15–6000	$\text{GY}_2\text{O}_3\text{R} = -1976462 + 731.6512 \cdot T - 121.881 \cdot T \cdot \ln(T) - 0.00506 \cdot T^2 + 1090000/T - 13000000/T^2$
298.15–6000	$\text{GY}_2\text{O}_3\text{H} = \text{GY}_2\text{O}_3\text{R} + 25100 - 9.654 \cdot T$
298.15–6000	$\text{GZYO} = 0.4286 \cdot \text{GZRO}_2\text{C} + 0.2857 \cdot \text{GY}_2\text{O}_3\text{R} - 14550.3912 - 0.520412688 \cdot T$
298.15–6000	

Fig. 1. Room temperature X-ray powder diffraction patterns of 16TaYSZ heat treated for 4 h at different temperatures (○: YTaO₄).Table 2
Variation of tetragonality of 20TaYSZ phase with temperature *T*.

<i>T</i> , °C	Tetragonality ^a
1100	1.0212
1200	1.0248
1300	1.0255
1400	1.0258
1500	1.0262

^a Tetragonality was calculated as $c/a\sqrt{2}$.

and tetragonality increases with the increase of YTaO₄ content. The 20TaYSZ sample corresponds to a system where ZrO₂ is doped with 20 mol% YTaO₄. The *c/a* value of this composition at 1500 °C is calculated to be 1.0262, what agrees well with the reported value elsewhere.²⁵ 20TaYSZ pretreated at 1500 °C remains stable when treated for 600 h at 1250 °C. Fig. 2 shows the XRD patterns of pretreated (at 1500 °C) 20TaYSZ sample which was later treated at 1250 °C for 4 h and 600 h. No phase change observed upon long term annealing at 1250 °C. However, some weak reflections at $2\Theta = 28.4$ and 58.8 can be seen. Though it is difficult to analyse these weak overlapping peaks but it can be m-YTaO₄ and/or orthorhombic Y₃TaO₇ and/or orthorhom-

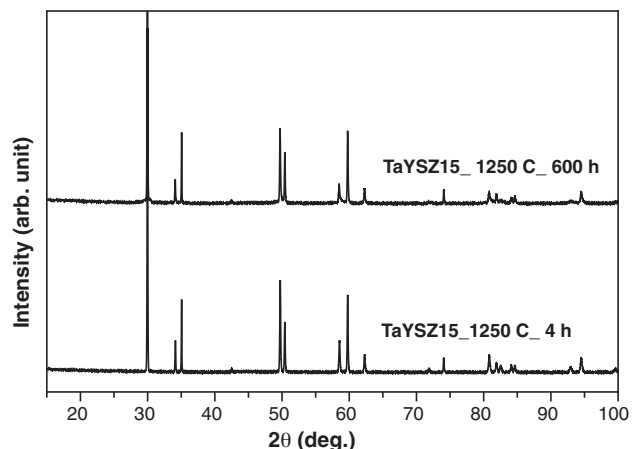


Fig. 2. Room temperature X-ray powder diffraction pattern of TaYSZ15 treated at 1250 °C for 4 h and 600 h.

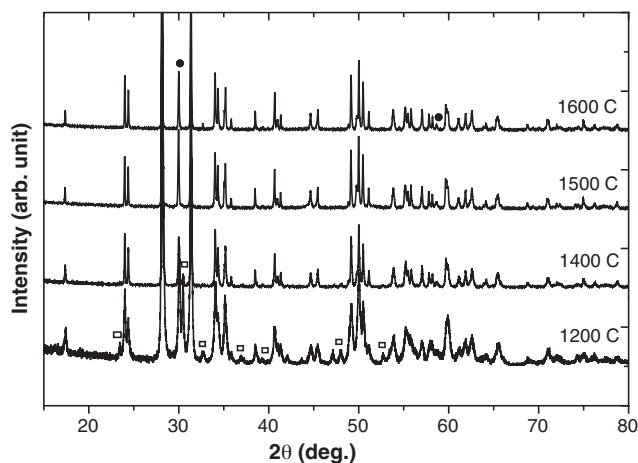


Fig. 3. Room temperature X-ray powder diffraction patterns of 10TaYSZ heat treated for 4 h at different temperatures (●: t-TaYSZ, ■: m-YTaO₄).

bic Y_{2.8}Ta_{1.17}O_{2.8} as found by search and match from ICSD database (www.icsdweb.fiz-karlsruhe.de).

Another composition prepared in this work was Y_{0.1}Ta_{0.1}Zr_{0.8}O₂ which corresponds to 11 mol% YTaO₄ doped ZrO₂. According to previous works^{5,25} this composition should correspond to t-ZrO₂ and m-ZrO₂ solid solutions at room temperature after being treated at 1500 °C. X-ray diffraction patterns of 11TaYSZ sample treated at different temperatures (Fig. 3) show that at all temperatures m-ZrO₂ ss ('ss' stands for solid solution) is the major phase with t-TaYSZ and m-YTaO₄ as the minor phases. Peaks corresponding to YTaO₄ phase can be seen up to 1400 °C. Above 1400 °C the YTaO₄ phase disappears.

Dissolution of YTaO₄ phase in the ZrO₂ lattice at and above 1400 °C in 20TaYSZ and 11TaYSZ systems is related to the transformation of monoclinic YTaO₄ into tetragonal YTaO₄ at that temperature. The resulted t-YTaO₄ has scheelite-like structure,²⁶ which enhances solubility of YTaO₄ in t-ZrO₂ above 1400 °C.

4.2. Preliminary thermodynamic description

The thermodynamic parameters of fluorite and tetragonal phases were assessed in the ZrO₂–Ta₂O₅ system to reproduce small solubility of Ta₂O₅ (~2 mol%) in these phases. The parameters of liquid phase were not optimised because phase diagram at high temperatures is not known. The calculated isothermal cross-section ZrO₂–Ta₂O₅ system is presented in Fig. 4.

The Gibbs energy of the YTaO₄ phase and the Gibbs energies and mixing parameters of Y₂O₃_C (cubic) phase were estimated to reproduce experimental solubility of Ta₂O₅ in the cubic Y₂O₃ phase and stability of the YTaO₄ phase up to high temperatures. Additionally, parameters of fluorite phase were estimated to comply with the stability of fluorite phase (Y₃TaO₇) at high temperatures. Calculated composition of the fluorite phase shifted in Y₂O₃ rich region. Probably, taking into account orthorhombic phases will improve the results. The parameters of liquid were not optimised due to the large uncertainty of experimental data

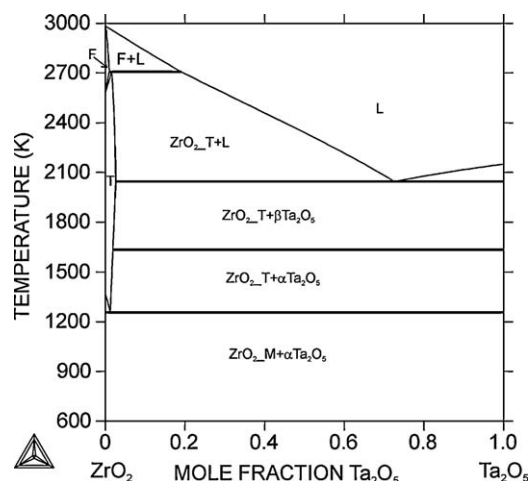


Fig. 4. Calculated isothermal section of the ZrO₂–Ta₂O₅ system.

at high temperatures. The mixing parameters of tetragonal phase were estimated to be close to the fluorite phase but with slightly more positive values assigned to them to avoid appearance of tetragonal phase in the Y₂O₃–Ta₂O₅ system. Calculated phase diagram of the Y₂O₃–Ta₂O₅ system is presented in Fig. 5.

The binary descriptions were combined in ternary. The ternary mixing parameter of tetragonal phase and the Gibbs energy of YTaO₄ were adjusted to agree with the experimentally indicated tie lines in ternary system and maximal solubility of Ta₂O₅ and Y₂O₃ in tetragonal phase. The calculated isothermal section of the ZrO₂–Ta₂O₅–Y₂O₃ system at 1500 °C is presented in Fig. 6a. The homogeneity range of tetragonal phase is narrow and extended in the direction of YTaO₄. Maximal content of Ta₂O₅ in fluorite structure reaches 4.5 mol %. The calculated phase diagram is in a reasonable agreement with experimental results obtained earlier.⁵ The isothermal section calculated at 1200 °C is presented in Fig. 6b. It is quite similar to phase diagram at 1500 °C. The calculated composition of tetragonal phase in equilibrium with YTaO₄ and Ta₂O₅ is practically the same for both temperatures. The contrast to isothermal section at 1500 °C are the δ-phase which is stable at 1200 °C, decreased maximal content of Ta₂O₅ in fluorite structure to 2.7 mol % and the com-

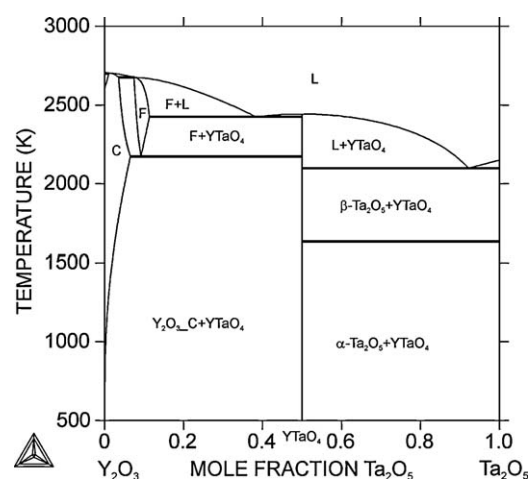


Fig. 5. Calculated phase diagram of the Y₂O₃–Ta₂O₅ system.

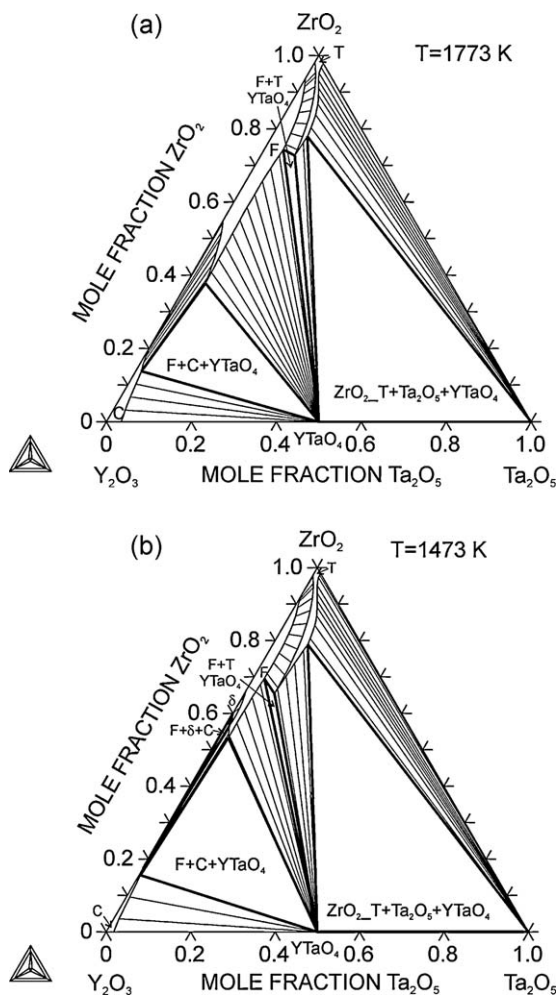


Fig. 6. Calculated isothermal section of the ZrO_2 – Ta_2O_5 – Y_2O_3 system at 1500 °C (a) and at 1200 °C (b).

position of tetragonal phase in equilibrium with fluorite structure and YTaO_4 changes with lower ZrO_2 and higher Y_2O_3 content compared to that at 1500 °C. It should be mentioned that temperature dependence of ternary mixing parameter was not optimised due to absence of reliable data on temperature dependence of maximal solubility of YTaO_4 in tetragonal phase. It is important to underline that the obtained thermodynamic description is preliminary and further improvement is required such as taking into account monoclinic phase of YTaO_4 and orthorhombic phase $\text{Ta}_2\text{Zr}_6\text{O}_{17}$. Measurement of thermodynamic properties for YTaO_4 and orthorhombic phase $\text{Ta}_2\text{Zr}_6\text{O}_{17}$ and including them into thermodynamic database should provide better fit of experimental data. On the other hand, the experimental studies at temperatures lower than 1500 °C indicate that equilibrium is not achieved and thus thermodynamic calculations will allow us to estimate equilibrium phase relation at lower temperatures.

5. Conclusion

The preliminary thermodynamic description of the ZrO_2 – Ta_2O_5 – Y_2O_3 system is derived showing phase relations at 1500 °C and at 1200 °C. Ternary diagram obtained here is in

good agreement with previously derived one at 1500 °C. The ternary phase diagram at 1200 °C has been derived here for the first time. The stability region of tetragonal solid solution (T) is almost unaffected by variation of temperature. This is also complimented from our experimental results. It has been shown that once YTaO_4 gets soluble in t- ZrO_2 at 1500 °C, this phase does not appear when annealed at low temperature for long duration. However, some weak reflections are about to appear upon long term annealing. Hence, experimental studies of thermodynamic properties of the YTaO_4 are highly necessary to get more exact thermodynamic parameters in the binary and ternary system. Further studies of the stability of orthorhombic phase in the ZrO_2 – Ta_2O_5 system and its thermodynamic properties are in due course. Information about phase composition of tetragonal and fluorite structure in ternary system at different temperatures is needed to make full assessment of thermodynamic parameters of these phases.

Acknowledgements

Authors are indebted to Innovation Promotion Agency (CTI) of Swiss Federal Office for Professional Education and Technology (Project 8974.1 PFIW-IW) for financial support.

References

- Levi CG. Emerging materials and processes for thermal barrier coatings. *Curr Opin Solid State Mater Sci* 2004;**8**:77–91.
- Jones RL, Mess D. Improved tetragonal phase stability at 1400 °C with scandia, yttria-stabilized zirconia. *Surf Coat Technol* 1996;**86**–**87**:94–101.
- Miller RA, Smialek JL, Garlick RG. *Science and technology of zirconia*. Columbus, OH: Am. Ceram. Soc., Inc.; 1981. p. 241.
- Pitek FM, Levi CG. Opportunities for TBCs in the ZrO_2 – $\text{YO}_{1.5}$ – Ta_2O_5 system. *Surf Coat Technol* 2007;**201**:6044–50.
- Kim DJ, Tien TY. Phase stability and physical properties of cubic and tetragonal ZrO_2 in the system ZrO_2 – Y_2O_3 – Ta_2O_5 . *J Am Ceram Soc* 1991;**74**:3061–5.
- Li P, Chen IW, Penner-Hahn JE. Effect of dopands on zirconia stabilization—An X-ray absorption study. III. Charge-compensating dopants. *J Am Ceram Soc* 1994;**77**:1289–95.
- Kim DJ. Effect of Ta_2O_5 , Nb_2O_5 and HfO_2 alloying on the transformability of Y_2O_3 -stabilised tetragonal ZrO_2 . *J Am Ceram Soc* 1990;**73**:115–20.
- Ho SM. On the structural chemistry of zirconium oxide. *Mater Sci Eng* 1982;**54**:23–9.
- Raghavan S, Wang H, Porter WD, Dinwiddie RB, Vassen R, Stoeber D, et al. $\text{Ta}_2\text{O}_5/\text{Nb}_2\text{O}_5$ and Y_2O_3 co-doped zirconias for thermal barrier coatings. *J Am Ceram Soc* 2004;**87**:431–7.
- TCC. *Thermo-Calc software*. Stockholm, Sweden: Stockholm Technology Park; 2006.
- Lukas H, Fries S, Sundman B. *Computational thermodynamics. The CAL-PHAD method*. Cambridge University Press; 2007.
- Roth RS, Waring JL. Effect of oxide additions on the polymorphism of tantalum pentoxide III. Stabilization of the low temperature structure type. *J Res Natl Bur Stand A: Phys Chem* 1970;**74A**, **4**:485–93.
- King, B.W., Schultz, J., Durbin, E.A. and Duckworth, W.H., Properties of Tantalum Systems. U.S.A.E.C., Report No. BMI-1106, 1956, 1–40.
- Zheng C, West AR. Compound and solid solution formation phase equilibria and electrical properties in the ceramic system ZrO_2 – La_2O_3 – Ta_2O_5 . *J Mater Chem* 1991;**1**, **2**:163–7.
- Bondar IA, Kalinin AI, Koroleva LN. Physico-chemical investigation of the system Y_2O_3 – Ta_2O_5 and the synthesis of single crystals of a number of tantalates. *Izv Akad Nauk SSSR, Inorg Mater (Engl Transl)* 1972;**8**, **10**:1649–50.

16. Vasil'ev VS, Pinaeva MM, Shkirman SF. *Russ J Inorg Chem (Engl Transl)* 1979;**24**, 4:578–82.
17. Yokogawa Y, Yoshimura M. High temperature phase relations in the system Y_2O_3 – Ta_2O_5 . *J Am Ceram Soc* 1991;**74**, 9:2077–81.
18. Yokogawa Y, Yoshimura M. Formation and stability regions of the high-temperature fluorite-related phases in the R_2O_3 – Ta_2O_5 system (R=La, Nd, Sm, Ho, Er and Yb). *J Am Ceram Soc* 1997;**80**, 8: 1965–74.
19. Yashima M, Tsuji T. Crystal structure, disorder, and diffusion path of oxygen ion conductors $Y_{1-x}Ta_xO_{1.5+x}$ ($x=0.215$ and 0.30). *Chem Mater* 2007;**19**, 14:3539–44.
20. Kim S, Yashima M, Kakihana M, Yoshimura M. Electrical properties of defect-fluorite phase in the system R_2O_3 – Ta_2O_5 (R = Gd, Y, Er and Yb). *J Alloys Compd* 1993;**192**:72–4.
21. Fabrichnaya O, Aldinger F. Assessment of thermodynamic parameters in the system ZrO_2 – Y_2O_3 – Al_2O_3 . *Z Metallkd* 2004;**95**:27–39.
22. Fabrichnaya O, Wang C, Zinkevich M, Levi CG, Aldinger F. Phase equilibria and thermodynamic properties of the ZrO_2 – $GdO_{1.5}$ – $YO_{1.5}$ system. *J Phase Equilib Diffus* 2005;**26**:591–604.
23. Fabrichnaya O, Zinkevich M, Aldinger F. Thermodynamic modelling in the ZrO_2 – La_2O_3 – Y_2O_3 – Al_2O_3 system. *Int J Mater Res* 2007;**98**, 9:838–46.
24. Hillert M. The compound energy formalism. *J Alloys Compd* 2001;**320**, 2:161–76.
25. Kim DJ, Hubbard CR. X-ray powder diffraction data for tetragonal zirconia solid solutions in system ZrO_2 – $YTaO_4$. *Powder Diffr* 1992;**7**:174–5.
26. Mather SA, Davies PK. Nonequilibrium phase formation in oxides prepared at low temperature: fergusonite-related phases. *J Am Ceram Soc* 1995;**78**:2737–45.